

# A Technique to Control Mercury From Flue Gas: The Thief Process



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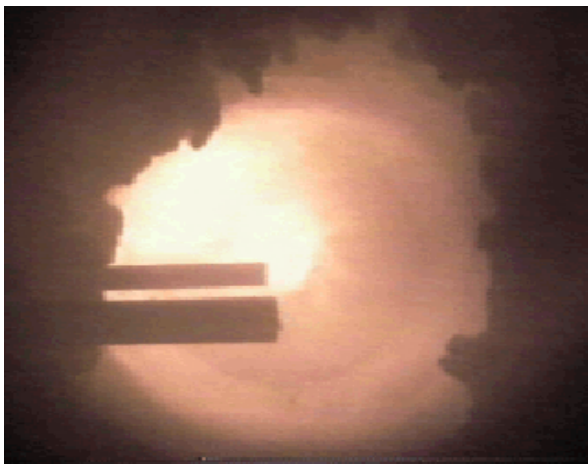
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# Furnace Sampling Probes



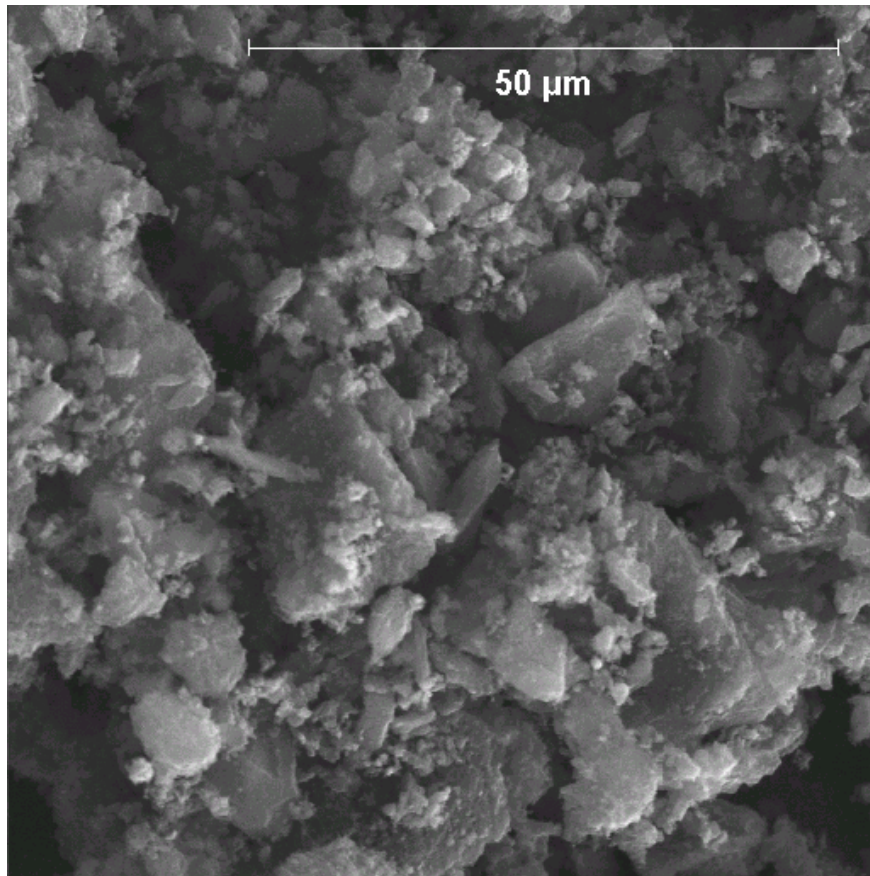
**NETL Borescope Probe**

View of Pulverized Coal Flame  
and Sampling Probes

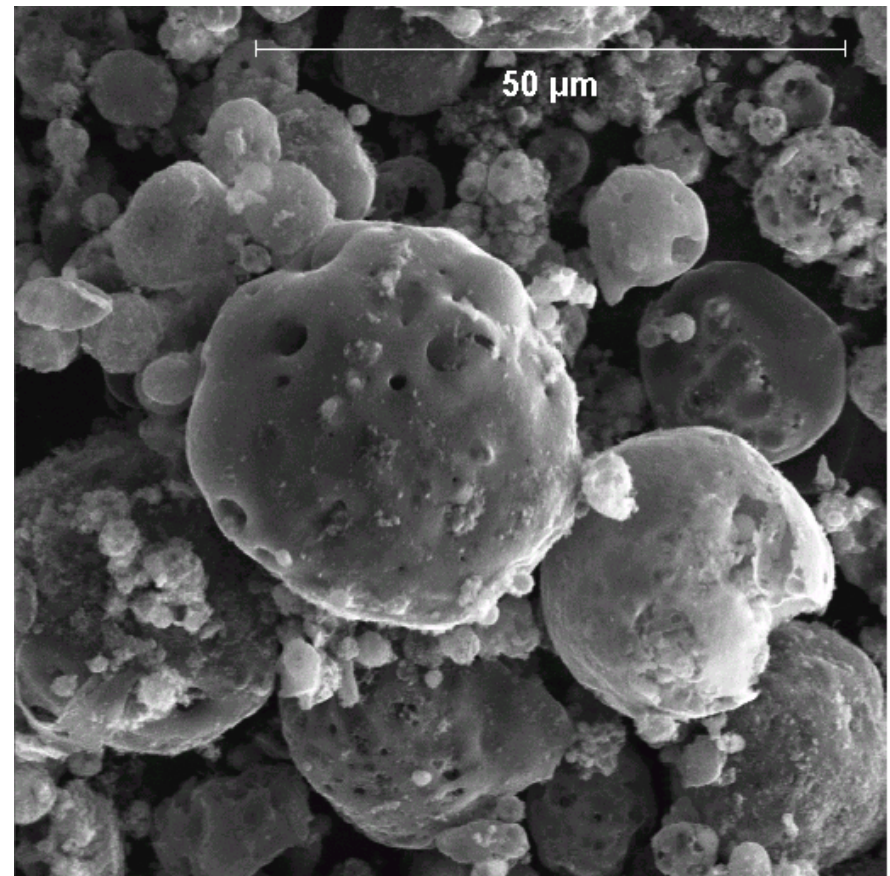


*Support – Conventional HVT, gas, and particulate sampling probes  
... Lab-scale screening of Thief samples for Hg reactivity*

## Norit Darco



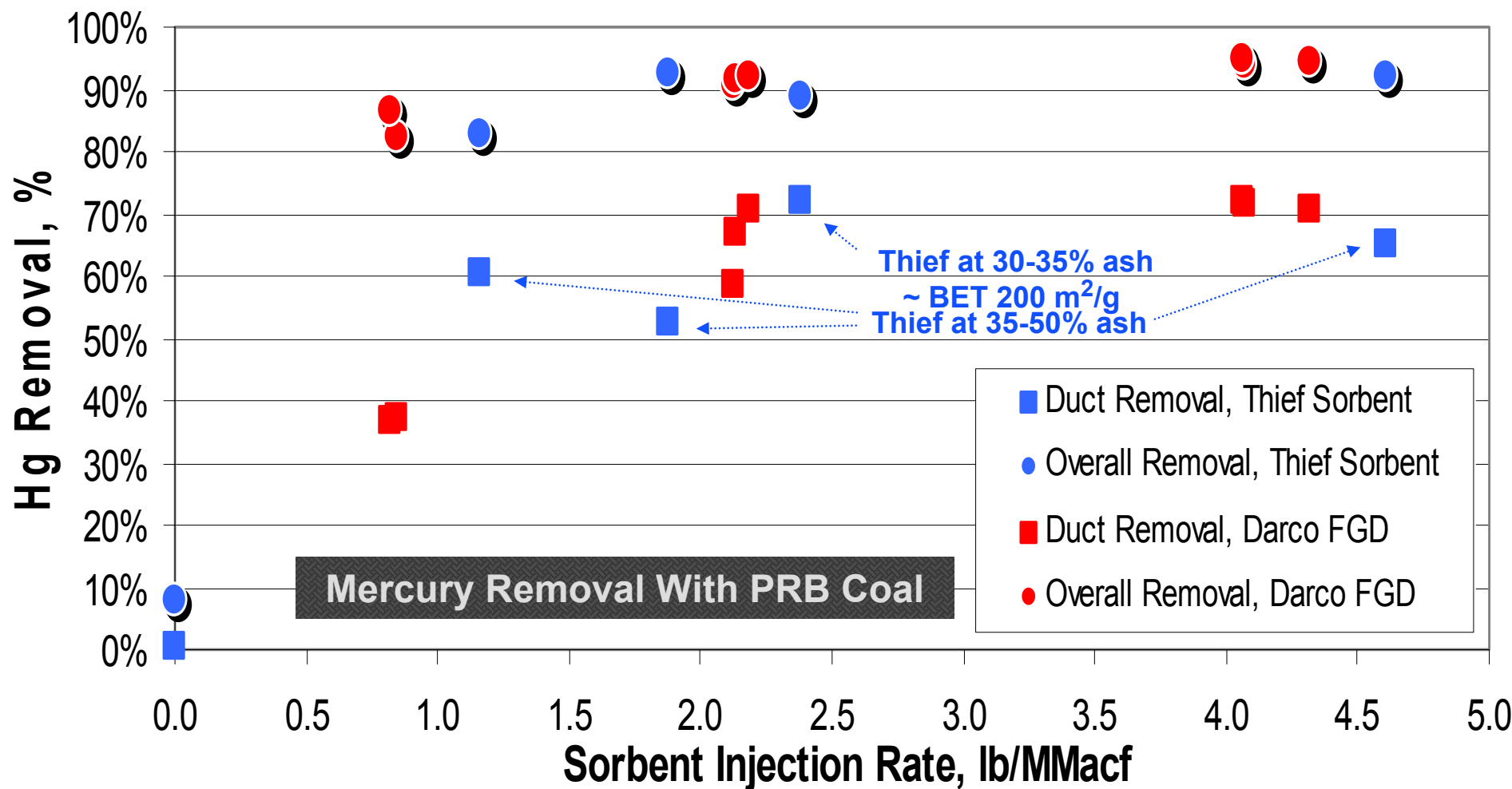
## Thief Sample



**Characterization** - Surface area (BET), pore volume, particle size, bulk chemical analysis, microanalysis

Mercury capacity in lab-scale screening

# Mercury Removal Results - Darco FGD vs. Thief Sorbent



Baghouse 270°F

Sorbent Duct Residence Time 2.5 sec



## Example Relationship of Particle Burnout & Furnace Gas during Combustion

**Semi-Combusted PRB**  
wt% basis

<b>Ash</b>	<b>20.1</b>	<b>24.7</b>	<b>32.0</b>	<b>37.5</b>	<b>45.4</b>	<b>51.9</b>	<b>60.6</b>
<b>Carbon</b>	<b>78.2</b>	<b>73.7</b>	<b>66.6</b>	<b>61.1</b>	<b>53.4</b>	<b>47.0</b>	<b>38.4</b>
<b>Other (S, N, O, H)</b>	<b>1.7</b>	<b>1.6</b>	<b>1.5</b>	<b>1.4</b>	<b>1.2</b>	<b>1.1</b>	<b>1.0</b>
 <b>Carbon Conversion, %</b>	 <b>57</b>	 <b>67</b>	 <b>77</b>	 <b>82</b>	 <b>87</b>	 <b>90</b>	 <b>93</b>
<b>Furnace Gas</b>							
<b>lb gas per lb particle</b>	<b>17</b>	<b>24</b>	<b>35</b>	<b>44</b>	<b>57</b>	<b>69</b>	<b>84</b>
<b>(ranges during</b>	<b>18</b>	<b>25</b>	<b>37</b>	<b>46</b>	<b>59</b>	<b>70</b>	<b>85</b>
<b>combustion)</b>	<b>21</b>	<b>29</b>	<b>41</b>	<b>50</b>	<b>62</b>	<b>71</b>	<b>86</b>

*Support Tools – CFD modeling, in-furnace sensors (LOI, CO, temperature) and conventional sampling probes ... lab-scale screening of Thief samples (for Hg reactivity) for site-specific boiler designs*



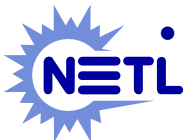


# Thief Process Equipment

- **Thief Process – engineering & field assembly of small components for slipstream**
  - Probe, including small boiler penetration
  - Duct work and insulation
  - Simple (e.g., double pipe) heat exchanger
  - ID Fan
  - Instrumentation and controls
  - *Optional* - baghouse/cyclone, small storage hopper, sorbent feeder ... for intermediate Thief sorbent collection/storage to add flexibility

*Engineering strategy for managing a small series of heat rate penalties (in lieu of sorbent purchases) is the key driver in Thief Process*

- **Thief Process**
  - Extraction of ~ 0.1 - 0.5% of furnace gas inside boiler
    - Much lower requirements than utility FGR experience or 3-5 MWe slipstreams built for field studies of flue gas cleanup technologies
    - Heat rate penalty  $\ll 0.5\%$



# Thief Process – Thermal Heat Rate Penalty

The thermal heat rate penalty basically consists of 3 items:

- **Combustible heat loss**, based on estimated heating value of Thief solids (e.g., unburned carbon loss\*14,500 Btu/lb, and adjusted for H, S, etc.)
  - Combustible heat loss includes Thief furnace gas – for example, where Thief gas contains appreciable quantities of carbon monoxide (4374 Btu/lb).
- **Sensible heat loss** when cooling the extracted Thief solids & gas through the system prior to re-injection
  - This is given by the calculated heat capacities of Thief gas composition (based on standard correlations) and estimate of Thief sorbent heat capacity
- **Additional heat losses**, the most important is the *incident heat transfer* from the furnace gas (boiler) to the high-temperature Thief probe
  - This is based on designing a probe to absorb a specified incident heat flux (Btu/hr-ft<sup>2</sup>), and surface area of probe (OD and length) inside the boiler

The latter two considerations influenced by engineering design in managing heat rate losses (e.g., tie-in with cooling water system, temperatures where extraction/re-injection occurs)



# Thief Process – Parasitic Power Requirements

- **Suction (e.g., fan power) for extraction of Thief sorbent/gas from the furnace and reinjection into downstream location**
  - This is calculated based on Thief gas requirements and pressure drop through various probe(s) and piping
- **Pneumatic injection if Thief sorbent is stored and handled similar to activated carbon ... if so, this is treated similar to the ACI case**
- **Pulverizer power required for make-up coal from thermal heat penalty**
  - Pulverizer power is specified on per ton coal basis, and a typical value for existing pulverizers is 22 kW-hr/ton coal
- **Parasitic power associated with circulating any heat exchanger cooling media (e.g., if a separate heat transfer system with new pumps, etc. would be purchased)**
  - Largely negligible if cooling is tied-into the power plant water system assuming existing system can handle minute changes in pressure head
    - Thief incremental cooling requirements are very small compared to the power station so that total water circulation is basically the same
    - Thief process basically diverts a minute fraction of the water flow through a system which may have slightly higher pressure drop due to the small scale of heat exchanger piping







## Example Heat Balance for Thief Process (at at 2 lb/MMacf) for 500 MW PRB Reference Plant

Thief Sorbent, wt% Ash	30.0	35.0	40.0	45.0
Thief Gas, lb gas per lb particle	34	42	51	59
Thief Sorbent, tons per year	796	796	796	796
Heat Rate Penalty - MMBtu/yr				
combustible heat loss	17,443	16,599	15,693	14,745
sensible heat loss	40,988	50,516	60,389	70,338
incident heat loss	15,088	16,771	18,352	19,819
sum	73,519	83,886	94,434	104,902
Coal Firing Rate - Trillion Btu/yr	37.3	37.3	37.3	37.3
heat rate penalty, %	0.22	0.26	0.29	0.32
With 70% Incident/Sensible Recovery				
heat rate penalty, % (adjusted)	0.10	0.11	0.12	0.13



## Example Parasitic Power Considerations for Thief Process (at 2 lb/MMacf) for 500 MW PRB Reference Plant

Thief Sorbent, wt% Ash	30.0	35.0	40.0	45.0
Thief Slipstream Duct Work				
Thief Gas Flow, lb/hr	8936	9581	11506	13445
Duct Pipe Size, inch	12	12	14	14
Parasitic Power - Thief Gas Suction				
Thief Gas Annual kW-hr	326,989	349,388	418,398	487,932
Parasitic Power - Pulverizer Coal Make-up				
Thief Coal Make-up Flow, ton per year	5394	5593	6291	6985
Annual Incremental Pulverizer kW-hr	118,668	123,046	138,402	153,670
Parasitic Power - ID Fan Increment				
Thief Gas Estimated Power, kW-hr	52,552	54,489	61,295	68,048
Parasitic Power - Thief Total, kW-hr	498,200	526,920	618,100	709,640
Parasitic Power Requirement, %	0.014%	0.015%	0.018%	0.020%



## Example Impact on Fly Ash for Thief Process (at 2 lb/MMacf) for 500 MW PRB Reference Plant

	wt% ash composition in Thief Sample				
	30.0	35.0	40.0	45.0	50.0
Incremental Increase in Fly Ash					
PRB Baseline LOI, wt%	0.2	0.2	0.2	0.2	0.2
Fly Ash Percent of Total CCB	80	80	80	80	80
Baseline Fly Ash tons/yr	94250	94250	94250	94250	94250
% Increase in Fly Ash	0.84	0.84	0.84	0.84	0.84
% LOI in Final Fly Ash	0.77	0.73	0.69	0.65	0.61

*Fly Ash Characteristics or Marketability Will be Studied in the Future  
(e.g., Perhaps During Scale-Up)*

*Thief Process does not introduce “external” substance in commingled fly ash*



# Thief Process Optimization FY05 Plans

- **Demonstrate Integrated, Continuous Testing**
  - Bypass cyclone collection and storage
    - Improved Hg removal expected with smallest Thief particles
- **Further refine Thief Process economics model**
  - Identify sensitivity options and target R&D opportunities
- **Thief sorbent characterization and 500 lb/hr furnace mapping on PRB coal, PRB blend, lignite**
  - Test Thief samples from other combustor locations & conditions
    - Obtain experimental data to evaluate sensitivities with cost model
  - Thief furnace gas characterization to enhance mapping studies and evaluate options for gas reinjection in concert with cost model
- **Support Thief licensing and scale-up**
  - Technical issues and business plan

